





HabEx Architecture Option A Overview

STDT Meeting #6

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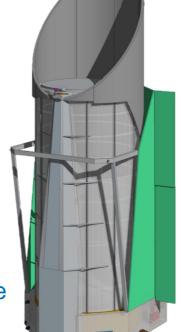
HabEx Architecture Option A



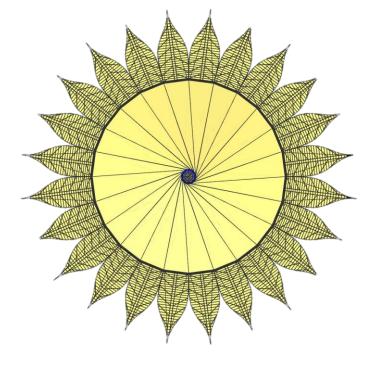
- Summary of Architecture Option A
- Key Design Features and Rationale
 - Vector Vortex Coronagraph

- 72-m Starshade

Microthrusters



72-meter diameter Starshade

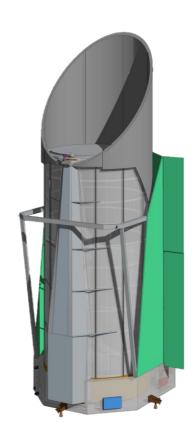


4-meter diameter aperture Telescope



Telescope Flight System (Baseline)



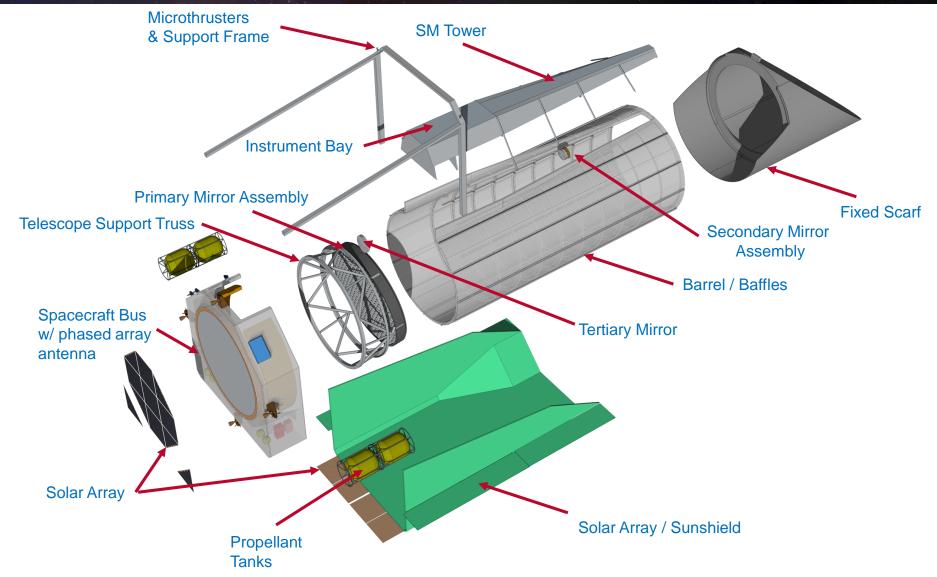


- 4-meter diameter aperture
- Off-axis, Three-mirror anastigmat telescope (unobscured)
- Four Instruments:
 - Coronagraph Imager/Spectrograph (CG)
 - Starshade Imager/Spectrograph (SS)
 - UV Spectrograph (UVS)
 - Workhorse Camera Imager/Spectrograph (HWC)
- Fine Guider Sensor (FGS)
- ACS Thrusters
- Microthrusters
- Solar Array/Sunshield
- Phased Array Antenna
 - Ka-band data downlink, 6.5Mbps
 - S-band cross-communications with Starshade



Telescope Flight System (Baseline) Exploded View

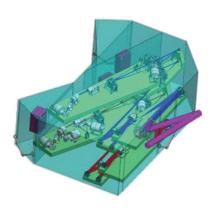


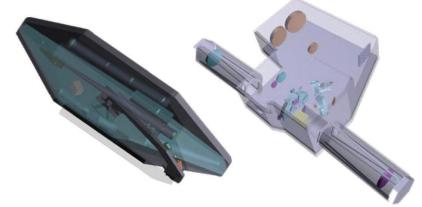




Instruments (Baseline)









	Coronagraph	Starshade	Workhorse Camera	UV Spectrograph
Purpose	Exoplanet imaging and characterization	Exoplanet imaging and characterization	Multipurpose, wide-field imaging camera and spectrograph for general astrophysics	High-resolution, UV spectroscopy for general astrophysics
Instrument Type	Vortex charge 6 coronagraph with: - Raw contrast: 1×10 ⁻¹⁰ at IWA - ∆mag limit = 26.0 - 20% instantaneous bandwidth Imager and spectrograph	72 m dia starshade occulter with: - 124,000 km separation - Raw contrast: 1×10 ⁻¹⁰ at IWA - ∆mag limit = 26.0 - 107% instantaneous bandwidth Imager and spectrograph	Imager and spectrograph	High-resolution spectrograph
Channels	Vis, Blue: 0.45–0.67 µm Imager + IFS with R = 140 Vis, Red: 0.67–1.0 µm Imager + IFS with R = 140 NIR: 0.95–1.8 µm, Imager + slit spectrograph with R = 40	UV: 0.2–0.45 µm Imager + grism with R = 7 Vis: 0.45–1.0 µm Imager + IFS with R = 140 NIR: 0.95–1.8 µm Imager + IFS with R = 40	UV: 0.15–0.4 µm Imager + grism with R = 2,000 Vis: 0.4–0.95 µm Imager + grism with R = 2,000 NIR: 0.95–1.8 µm Imager + grism with R = 2,000	UV: 0.115–0.3 µm (20 bands), R = 60,000; 25,000; 12,000; 6,000; 3,000; 1,000; 500
Field of View	FOV: 1.5×1.5 arcsec ² @ 0.5 μm IWA: 2.4 λ/D = 62 mas @ 0.5 μm OWA: 0.74 arcsec @ 0.5 μm	FOV: 11.9×11.9 arcsec ² (Vis) IWA: 60 mas (0.3–1.0 µm) OWA: 6 arcsec (Vis)	3×3 arcmin ²	3×3 arcmin ²
Features	64×64 deformable mirrors (2) Low-order wavefront sensing & control	Formation flying sensing & control	Microshutter array for multi-object spectroscopy 2×2 array, 171×365 apertures	Microshutter array for multi-object spectroscopy 2×2 array, 171×365 apertures





Starshade Flight System (Baseline)



72-meter diameter (tip-to-tip)

40-meter diameter central disk 16-meter petals (x22)

Solar Electric Propulsion (SEP) Hall Effect thrusters

2 flight + 1 spare, each side (6 total)

Bi-prop hydrazine thrusters

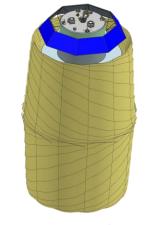
ACS

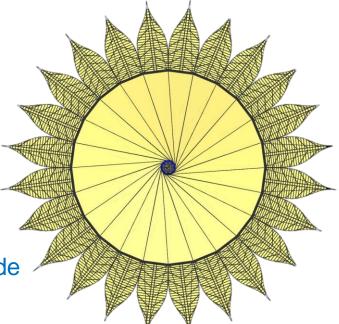
Orbit maintenance

Communications

X-band to ground, 1kbps, command & ranging

S-band to telescope, 100bps, data transfer & ranging





72-meter diameter Starshade

Hobex



Starshade Flight System (Baseline) Exploded View



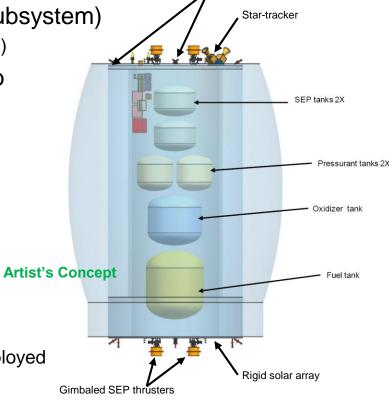
72m diameter Starshade deploys radially from Hub exterior

PLUS (Petal Launch Restraint & Unfurler Subsystem)

deploys the Starshade occulter (jettisoned after use)

Starshade Bus fits within the Starshade Hub

- Bus Includes:
 - Solar Electric Propulsion (SEP) Hall effect thrusters
 - 2 Flight / 1 Spare (on each end)
 - Bi-prop chemical thrusters
 - Communications, with ground & telescope
 - Formation Flying beacon
 - Electronics
 - Solar Array (2 sets)
 - 1 rigid array on end of hub
 - 1 flexible CIGS array starshade disc when deployed
 - Thermal Control
- Starshade is spin-stabilized at 0.33 RPM
 - allows starshade occulter temperature to be passively controlled
- Communications same as telescope (w/o extra 1Tb storage)



Bi-prop thrusters



Why Vector Vortex Coronagraph?



Purpose:

 to maximize planet light throughput and contrast and minimize requirements on the telescope

Rationale:

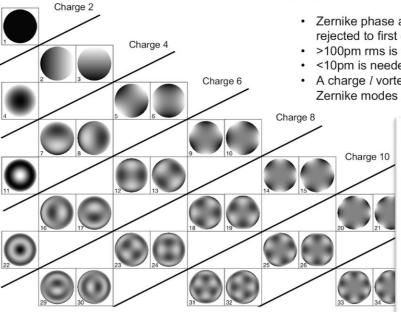
- Vector Vortex Coronagraphs exhibit very good performance on par (theoretically) with HLC or other coronagraph types
- Have been demonstrated in the lab and on ground-based telescopes (though not to the level required for space)
- VVCs are more forgiving on the telescope wavefront error stability by rejecting much of the lowest order Zernike WFE terms. These lowest terms are directly related to rigid body stability of the telescope optics as well as thermal bending modes.



VVC Null Space



The null space of a vortex coronagraph



Zern M1 **M2 M3** Mode (pm rms) (pm rms) (pm rms) focus z4 2000.0 500.0 500.0 z5 200.0 100.0 100.0 astig astig z6 200.0 100.0 100.0 coma z7 150.0 100.0 100.0 z8 150.0 100.0 100.0 comal trefoil z9 2.4 1.0 0.5 0.2 trefoil z10 0.2 0.2 spherical z11 100.0 100.0 100.0 2 astig z12 0.2 0.2 0.2 0.2 2 astig z13 0.2 0.2 z14 0.2 0.2 quadrafoil 0.2 0.2 0.2 0.2 quadrafoil z15 z16 0.2 0.2 0.2 2 coma 0.2 0.2 0.2 2 comal z17

- Zernike phase aberrations above the line are rejected to first order.
- >100pm rms is tolerable for null space modes.
- <10pm is needed for other modes up to ~Z₇₀.
- A charge / vortex coronagraph has (1/2)²
 Zernike modes in it's null space.

Garreth Ruane, Dimitri Mawet, Bertrand Mennesson, Jeffrey B. Jewell, Stuart B. Shaklan, "Vortex coronagraphs for the Habitable Exoplanet Imaging Mission concept: theoretical performance and telescope requirements," Journal of Astronomical Telescopes, Instruments, and Systems 4(1), 015004 (28 March 2018). https://doi.org/10.1117/1.JATIS.4.1.015004 Submission: Received 14 November 2017; Accepted 9 March 2018

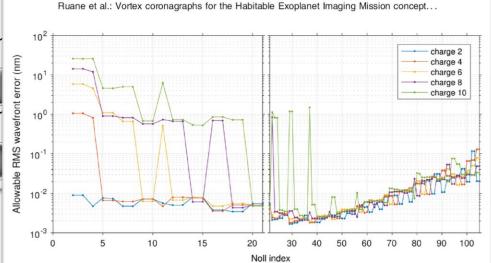


Fig. 4 Wavefront error requirements in the Zernike mode basis. The maximum allowable RMS wavefront error generates a normalized irradiance of 2×10^{-11} at an effective separation of $3\pm 0.5\,\lambda/D$ for $\lambda=450$ nm. The Zernike modes are ordered by Noll index to conform to conventions in astronomy. However, the wavefront error tolerance depends more naturally on the sum of indices n+|m|. As the charge increases, large wavefront errors (>100 pmrms) may be tolerated on more of the low-order aberrations. We have emphasized the lowest 21 modes, many of which tend to dominate the wavefront error budget and may be readily suppressed by vortex coronagraphs. The requirements for noll indices >40 are roughly the same for all charges \leq 10.

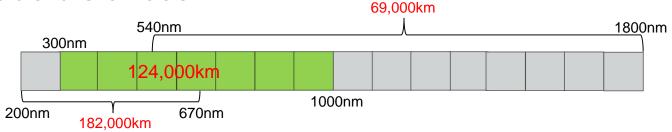
Example telescope optics WFE stability allocations



Why 72-m Starshade?



- Starshade IWA selected to match coronagraph at 500nm
 - $IWA = 2.4 \lambda/D = 62 mas$
- Starshade diameter requirements:
 - 300nm 1000nm at a single distance
 - IWA = 60mas at the tip (+margin)
 - Fresnel #10.5
- Starshade dimensions:
 - 40m diameter central disk
 - 16m long petals (quantity: 22)
- Starshade distances:





Why Microthrusters?



Purpose:

to offset solar pressure which imparts torque on the telescope.

Background:

- Solar pressure is 0.5μN/m² at Sun-Earth L2.
- HabEx has ~100m² projected area,
- Solar pressure is $\sim 50 \mu N$, with about a 3-4m offset from the center of mass.

Rationale:

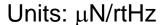
- Microthrusters have sufficient thrust (single thruster ≤ 30μN on ST7)
- Has very good thrust resolution (≦0.1μN)
- Likely higher reliability than reaction wheels (to be tested to confirm, but reaction wheels have had high profile failures)
- Likely significantly less noise than reaction wheels (≤0.03µN/rtHz over all frequencies) See next slide.

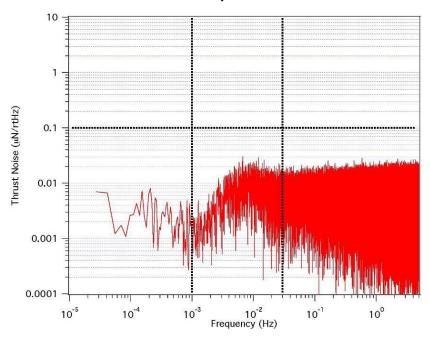




Microthruster noise vs Reaction Wheels



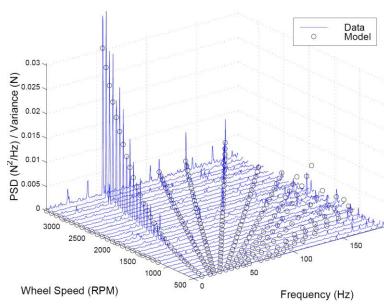




Thruster noise PSD plot for colloidal microthrusters. Max noise above 10⁻³ is likely due to thrust-balance sensor noise limits.

(ref: "Colloid Micro-Newton Thrusters For Precision Attitude Control", John Ziemer, et. al, April 2017, CL#17-2067)

Units: N²/Hz



Waterfall plot derived from measured data showing Ithaco Bwheel Fx data and the radial force model (reference: "Conditioning, Reduction, and Disturbance Analysis of Large Order Integrated Models for Space-Based Telescopes" By Scott Alan Uebelhart, MIT 2001)



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